



# A Handbook on

# Electrical Engineering



Contains well illustrated formulae & key theory concepts



**ESE, GATE, PSUs** 

& OTHER COMPETITIVE EXAMS





#### **MADE EASY Publications Pvt. Ltd.**

**Corporate Office:** 44-A/4, Kalu Sarai (Near Hauz Khas Metro Station), New Delhi-110016

Contact: 9021300500

E-mail: infomep@madeeasy.in

Visit us at: www.madeeasypublications.org

#### A Handbook on Electrical Engineering

© Copyright, by MADE EASY Publications Pvt. Ltd.

All rights are reserved. No part of this publication may be reproduced, stored in or introduced into a retrieval system, or transmitted in any form or by any means (electronic, mechanical, photo-copying, recording or otherwise), without the prior written permission of the above mentioned publisher of this book.



First Edition: 2012 Second Edition: 2014 Third Edition: 2015 Fourth Edition: 2019

Reprint: 2020 Reprint: 2021

Fifth Edition: 2022

Sixth Edition: 2023

# Director's Message



During the current age of international competition in Science and Technology, the Indian participation through skilled technical professionals have been challenging to the world. Constant efforts and desire to achieve top positions are still required.

I feel every candidate has ability to succeed but competitive environment and quality guidance is required to achieve high level goals. At MADE EASY, we help you discover your hidden talent and success quotient to achieve your ultimate goals. In my opinion CSE, ESE, GATE & PSUs exams are tools to enter in to the main stream of Nation serving. The real application of knowledge and talent starts, after you enter in to the working system. Here at MADE EASY you are also trained to become winner in your life and achieve job satisfaction.

MADE EASY alumni have shared their winning stories of success and expressed their gratitude towards quality guidance of MADE EASY. Our students have not only secured All India First Ranks in ESE, GATE and PSUs entrance examinations but also secured top positions in their career profiles. Now, I invite you to become an alumnus of MADE EASY to explore and achieve ultimate goal of your life. I promise to provide you quality guidance with competitive environment which is far advanced and ahead than the reach of other institutions. You will get the guidance, support and inspiration that you need to reach the peak of your career.

I have a true desire to serve the Society and the Nation easing path of the education for the people of India.

After a long experience of teaching Electrical Engineering over a period of time, MADE EASY team realised that there is a need of a good *Handbook* which can provide the crux of Electrical Engineering in a concise form to the student to brush up the formulae and important concepts required for ESE, GATE, PSUs and other competitive examinations. This *handbook* contains all the formulae and important theoretical aspects of Electrical Engineering. It provides much needed revision aid and study quidance before examinations.

**B. Singh** (Ex. IES) CMD, MADE EASY Group

# A Handbook on

# **Electrical Engineering**

Ch	apter 1 :	V.	Phase Controlled Rectifiers	128
Po	wer Systems 1-49	VI.	Choppers	143
l.	Supply System1	VII.	Inverters	149
II.	Line Parameters3		. AC Voltage Controllers	
III.	Performance of Transmission Line 13	IX.	Electric Drives	160
IV.	Concept of Corona21	Ch	apter 4 :	
V.	Mechanical Design of Overhead Lines23	Me	easurements and strumentation16	2-206
VI.	Balanced and Unbalanced Faults 25	ı.	Characteristics of Instruments a	
VII.	Power System Stability30		Measurement Systems	162
VIII.	Power System Transients32	II.	Circuit Components (Resistors,	
IX.	Economic Load Dispatch37		Inductors, Capacitors)	167
Χ.	Underground Cable38	III.	Galvanometers	169
XI.	Protective Relays42	IV.	Analog Meters	171
XII.	Circuit Breakers45	V.	Instrument Transformers	178
XIII.	Generating Power Stations46	VI.	Measurement of Power	
XIV.	Loads and Load Curves48		and Wattmeters	181
		VII.	Measurement of Resistance	185
Chapter 2:			. A.C. Bridges	191
Ele	ectrical Machines 50-102	IX.	Magnetic Measurements	196
l.	Transformers50	Χ.	Electronic Instruments	197
II.	Electromagnetic System63	XI.	Cathode Ray Oscilloscope	198
III.	Basic Concepts in Rotating	XII.	High Frequency Measurements	201
	Electrical Machines64	XIII	. Transducers	202
IV.	D.C. Machines66	XIV	. Digital Instrumentation	204
V.	Polyphase Induction Motors76			
VI.	Polyphase Synchronous Machines 85	Ch	napter 5:	
VII.	Single Phase Induction Machine 97	Ne	etwork Theory20	7-241
VIII.	Special Machines102	l.	Basic Definitions & Circuits Elemen	nt207
		II.	Network Laws and Theorems	215
	apter 3:	III.	Graph Theory	221
Power Electronics103-161			Laplace Transform Analysis	
l.	Power Electronics103		and Circuit Transients	
II.	Thyristor109	V.	Resonance	
III.	Thyristor Commutation	VI.		
	Techniques116	VII.	Two Port Network	234
IV.	Diode Circuits and Rectifiers121	VIII	Miscellaneous	237

Chapter 6 :	Cl	napter 9 :	
Control Systems242	2-276 D	igital Electronics 371	-422
. Introduction		Number System and Codes	
I. Mathematical Modelling		Logic Gates	
II. Transfer function	249	Boolean Algebra and	570
V. Time Response Analysis of C.S	254	Reduction Techniques	383
/. Stability in Time-Domain	261 IV.		
/I. Industrial Controller		Sequential Circuits	
/II. Compensator	267 VI.	·	
/III. Frequency Response Analysis	269	3	
X. State Space Analysis	2/5	. Counters	
Chanta 7		I. Digital ICs Family	
Chapter 7:		DACs and ADCs	
Signals and Systems 277		Miscellaneous	418
. Introduction to Signals			
I. Linear Time Invariant Systems		napter 10:	
II. Fourier Series	LI	ectrical Materials 423	-449
V. Fourier Transform	1.	Dielectric Properties of	
V. Laplace Transform		Insulating Materials	423
/I. Discrete Time Fourier Transform.	11.	Dielectric Breakdown	431
/II. Z-Transform	111.	Magnetic Properties	
/III. Discrete Fourier Transform		of Materials	433
X. Digital Filters	IV.	Conductive Materials	438
X. Miscellaneous	306 V.	Semiconductors	442
	VI.	Insulating Materials	443
Chapter 8 :	VII	. Structure of Materials	446
Analog Electronics 309	9-370 VII	I. Ceramic Materials	448
. Semiconductor Physics	200	napter 11 :	
I. Junction Diode Characteristics	317	ectromagnetic	
II. BJT Characteristics	327 <b>T</b> l	neory450	-449
V. Transistor Biasing Circuits		Vector Calculus	
/. BJT as an Amplifier	337	Cartesian Coordinate System	
/I. Junction Field Effect Transistors .		& Vector Calculus	451
/II. Metal Oxide Semiconductor	III.	Electrostatics	
Field Effect Transistor	343	Magnetostatics	
/III. Transistor Hybrid Model	346	Time-Varying Electromagnetic	
X. Feedback Amplifiers	348	Fields	469
X. Operational Amplifiers	\/I	Electromagnetic Wave	
KI. Large Signal Amplifiers	360 VI.	Propagation	472
XII. The Signal Generators and Wave Shaping Circuits	363 VII	. Transmission Lines	
VVAVE MIADING CITCUIS	)(1)		

Wave Shaping Circuits......363

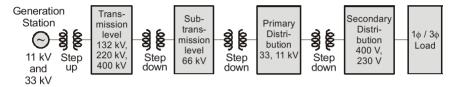
Chapter 12:			Analog Modulation530
Microprocessors484-526		IV.	Pulse Modulation537
l.	Introduction484	V.	Digital Carrier Modulation540
II.	Architecture of 8085485	VI.	Random Variables and Noise543
III.	Instruction Set and Data Formats492		
IV.	Interrupts508	Ch	napter 14:
V.	Interfacing with Microprocessor510	Co	omputer
VI.	Introduction to 8086514	Fu	ndamentals 547-571
VII.	Microcontroller518	I.	Data Representation547
		II.	Computer Architecture548
Chapter 13:		III.	Memory Organization553
Communication		IV.	Networking Fundamental562
Systems527-546			, and the second
I.	Basics527	V.	Programming Elements563
II.			Operating System Concepts564
	and Signals528		

1

# **Power Systems**

# **Supply System**

# **Basic Structure of Power System**

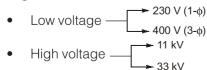


- Generating stations are interconnected by the lines.
- Transmission lines, when interconnected with each other, becomes transmission networks.
- The combined transmission and distribution network is known as the "power grid".

# Effect of System Voltage on Transmission of Power

- Power loss in the line is inversely proportional to the system voltage and power factor both.
- Percentage voltage drop in resistance decreases with the increase in the system voltage.
- Weight of the conductor material for the line will decreases with the increase in supply voltage and power factor.
- Efficiency of transmission, increases with the increase of supply voltage and power factor.
- Higher supply voltages also enhances the system stability.
- The problems encountered with high voltages are the insulation of the equipment, corona, radio and television interference.
- The voltage level of a system is therefore governed by the amount of power to be transmitted and the length of the line.

# **Voltage Level**



- Extra high voltage: 66 kV, 132 kV, 220 kV.
- Modern EHV: 400 kV
- Ultra high voltage: 765 kV and above.

#### **Conductor Used for Transmission Line**

- Copper conductor
- ACSR: Aluminium conductor steel reinforced.
- ACAR: Aluminium conductor alloy reinforced.
- AAAC : All Aluminium alloy conductor.
- Expanded ACSR conductor: Normally used for EHV lines.
- AAC : All Alluminium conductors.

# **Types of Conductor**

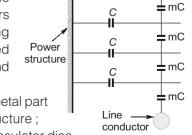
- Solid conductor: It has high skin effect.
- Hollow conductor: Preferred under heavy current, i.e., more than 1000 Amp.
- Stranded conductor.
- Composite standard conductor: used for voltage ≤ 220 kV.
- Bundle conductor: Used for voltage > 275 kV.

#### **Advantage of Bundle Conductor**

- Self distance (GMR) increased without change in mutual distance.
- Voltage gradient reduced so corona loss reduce.
- It reduces the interference with nearby communication line.
- Inductance (L) of transmission line reduces and capacitance (C) increases.
- Surge impedance, i.e.,  $Z_s = \sqrt{\frac{L}{C}}$  decreases.
- Power system stability increases.

# **Insulators**

Over head line insulators provide the required insulation to the line conductors from each other and from the supporting structures electrically. Most commonly used materials are porcelain, toughened glass and steatite.



Cross arm

where,  $C \rightarrow$  Capacitance between metal part of the insulator and tower structure;  $mC \rightarrow$  Capacitance of each insulator disc.

mC > C

#### Note:

 $\ensuremath{\square}$  The stress experienced by the disc near the power conductor is more than the stress experience by the disc near the cross-arm.

# **String Efficiency**

String efficiency = 
$$\frac{\text{Voltage across the whole string}}{n \times (\text{Voltage across the unit adjacent to line conductor})}$$

where,  $n \rightarrow \text{Number of insulator discs in the string}$ 

String efficiency also defined as

$$\%\eta = \frac{\text{Flashover voltage of the string}}{n \times \text{flashover voltage of one string}} \times 100$$

#### Note:

#### Methods of Equilising Potential Across Each Disc

- Increase the length of cross arm.
- Capacitance grading or grading of units.
- Use of grading rings or static shielding.

# Remember:

 $\ensuremath{\,^{\square}}$  For static shielding the capacitance from the shield to the  $K_{\rm th}$  link from the top

$$C_K = \frac{KC}{n-K}$$
 (::  $n = \text{number of disc}$ )

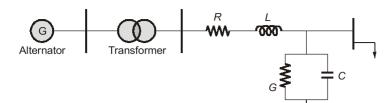
.....

# **Types of Insulator**

- Pin type insulator: Pin type insulator operate satisfactory upto 25 kV.
- Multipine type insulator: Operates upto 33 kV
- Suspension type insulator: A suspension insulator is designed to operate at 11 kV.
- Strain type insulator: Strain type insulator mechanically strong. It is used when direction of transmission line changes across river crossing and at the dead end of the transmission line.
- Shackle type: Shackle type insulator are used in low tension cable. These insulator can be operated either horizontally or vertically.

# II Line Parameters

Transmission line is a carrier on which bulk amount of power from a remote generating station to the operative areas is being carried out.



Transmission line is

- series combination of resistance (R) and inductance (L) and
- Parallel combination of shunt conductance (G) and capacitance (C).

#### Note:

- The line parameter of transmission line is calculated in per unity or per km and are constant for entire line length.
- The shunt conductance is caused by leakage current.
- In transmission line if G = 0 means leakage current is assume to be zero.
- Power loss in the conductor is only due to series resistance.
- Power transmission capacity of the line is mainly governed by the series inductance.

• Resistance of a conductor,  $R_{\text{eff}} = \frac{\text{Power loss in conductor}}{I^2}$  ohms

where,  $R_{\rm eff} \rightarrow$  Effective resistance of the conductor

D.C. Resistance of a Conductor, R<sub>dc</sub> = ρ l/A ohms
 where, ρ → Resistivity of conductor, Ω-m; I → Length of conductor, metre: A → Cross-sectional area. m²

#### Note:

☑ The effective resistance is equal to the dc resistance of the conductor only if the current is uniformly distributed throughout the cross-sectional area of the conductor (i.e. for DC only).

.....

#### Skin Effect

If DC is passed in a conductor, the current density is uniform over the cross-section of the conductor but when an alternating current flows through a conductor, the distribution tends to become non uniform. There is a tendency of the current to crowd near the surface of the conductor. This phenomenon is called "skin effect". The effective conductor resistance increases in AC as compared to DC which causes larger power loss.

#### ◀

# Remember: ....

Skin effect increases with increase in frequency, conductor diameter and permeability.

# **Proximity Effect**

When two or more conductors are in proximity, their electromagnetic field interact with each other, with the result that the current in each of them is redistributed such that the greater current density is concentrated in that part of the strand most remote from the interfering conductor. In each case, a reduced current rating results from the apparent increase of resistance.

#### Remember:

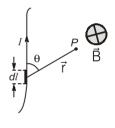
 $\ensuremath{\square}$  Proximity effect is more pronounced in case of cable, large conductors and high frequencies.

# **Magnetic Flux Density**

#### Biot-savart's law

 Magnetic flux at any point produced by a current carrying element

$$d\vec{B} = \frac{\mu}{4\pi} \frac{I d\vec{l} \times (\vec{r})}{r^3}$$



where,  $dB \rightarrow Infinitesimal flux density at point P$ 

 $I \rightarrow \text{Current in element}$ ;  $dl \rightarrow \text{Length of element}$ 

 $\theta \rightarrow$  Angle between current direction and radius vector to P

 $r \rightarrow \text{Radius vector}$ ;  $\mu \rightarrow \text{Permeability of medium}$ 

Magnetic flux density B at any point to an infinite conductor.





where, R = Radial distance of the point from the conductor.

# Note:

The direction of the flux density is normal to the plane containing the conductor and radius vector *R*.

Amperes's law , 
$$\boxed{\oint H.dl = I_{\text{enclosed}}}$$

where.

*H* → Magnetic field intensity

 $I \rightarrow R.M.S.$  value of current enclosed by an amperian loop.

#### **Relation Between Magnetic Flux Density and Magnetic Field Intensity**

$$B = \mu H$$
,  $\mu = \mu_0 \mu_r$ 

where.

 $\mu_0 \rightarrow 4\pi \times 10^{-7}$  H/m = Permeability of free space

 $\mu_r \to \text{Relative permeability of the medium}$ 

= 1 (for non magnetic material)

#### **Inductance**

Inductance of an inductor is the ratio of its total magnetic flux linkages to the current I through the inductor.

$$L = \frac{N\Psi_m}{I} = \frac{\lambda}{I}$$
 Henry

where.

 $\Psi_m \rightarrow$  Magnetic flux linkages through a single turn

 $N \rightarrow \text{Total number of turns}$ ;  $\lambda \rightarrow \text{Total magnetic flux linkages}$ 

Above formulae is valid for a medium in which the permeability is constant.

#### Remember: .....

The permeability of ferrous medium is not constant. For such cases the inductance is defined as the ratio of infinitesimal change in flux linkage to the infinitesimal change in current producing it

$$L = \frac{d\lambda}{dI}$$
 Henry

• Flux linkages within the conductor :  $\Psi_{int} = \frac{\mu I}{8\pi}$  Wb-T/m

where,  $\Psi_{\text{int}} \rightarrow \text{Total internal flux linkages}$ ;  $I \rightarrow \text{R.M.S. value of current}$ .

$$\Psi_{int} = 0.5I \times 10^{-7} \text{ Wb-T/m}$$

• Inductance of the conductor, contributed by flux within the conductor:

$$L_{\text{int}} = 0.5 \times 10^{-7} \text{ H/m}$$
 as  $L_{\text{int}} = \frac{\Psi_{\text{int}}}{I}$ 

• Flux linkages outside the conductor

$$\Psi_{12} = \frac{\mu I}{2\pi} \ln \left( \frac{D_2}{D_1} \right) \text{ Wb-T/m}$$

for 
$$\mu_r = 1$$
:  $\Psi_{12} = 2 \times 10^{-7} \ln \left( \frac{D_2}{D_1} \right)$  Wb-T/m

where  $\Psi_{12} \rightarrow$  Total flux linkages between points 1 and 2

Inductance of the conductor, contributed by flux between points 1 and 2:

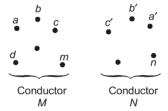
$$L_{12} = 2 \times 10^{-7} \ln \left( \frac{D_2}{D_1} \right) \text{ H/m}$$

• Inductance of a single phase two wire line:  $L = 4 \times 10^{-7} \ln \left( \frac{D}{r'} \right)$  H/m

where,  $D \rightarrow$  Distance between two solid conductors of same radii r  $r' \rightarrow$  Radius of fictitious conductor = 0.7788 r

#### **Inductance of Composite Conductor Lines**

Conductor M consists of m similar parallel sub-conductors and conductor N consists of n similar parallel sub-conductors.



#### (Single phase line having composite conductors)

If line current is I, then each strand of conductor M carries a current I/m and each strand of conductor N carries a current of -I/n (the conductor N being the return conductor).

$$L_{M} = 2 \times 10^{-7} \times ln \frac{\left[ \left( D_{aa'} D_{ab'} ... D_{an} \right) \left( D_{ba'} D_{bb'} ... D_{bn} \right) ... \left( D_{ma'} D_{mb'} ... D_{mn} \right) \right]^{1/mr}}{\left[ \left( D_{aa} \ D_{ab} ... D_{am} \right) \left( D_{ba} \ D_{bb} \ ... D_{bm} \right) ... \left( D_{ma} \ D_{mb} ... D_{mm} \right) \right]^{1/m^{2}}} \ H/m$$

where,  $L_M \rightarrow$  inductance of conductor M

$$L = 2 \times 10^{-7} \ln \left( \frac{\text{GMD}}{\text{GMR}} \right)$$

# Remember: .....

- GMD =  $mn^{th}$  root of the product of mn distances (known as the geometric mean distance between conductor M and conductor N and denoted by  $D_m$ ).
- GMR =  $(m^2)^{\text{th}}$  root of the product of  $m^2$  distances these being the distances from each sub-conductor of conductor M to every other sub-conductor of conductor M (including  $D_{aa'}$ ,  $D_{bb}$ .... $D_{mm}$ ).
- GMR = Geometric mean radius (denoted by D<sub>s</sub>), which depends on radius of conductors and does not effected by unequal spacing of conductors.
- $D_{aa} = 0.7788$  times the radius of sub-conductor 'a'.

# Inductance of 3-\phi Line With Equivalent Spacing.

Assuming balanced currents, i.e.,  $(I_a + I_b + I_c = 0)$ 

$$L_a = 2 \times 10^{-7} \ln \left( \frac{D}{r'} \right) \text{ H/m}$$

where.

 $L_a \rightarrow Inductance of phase$ 

 $D \rightarrow$  Distance between any two phases

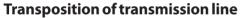
 $r' \rightarrow 0.7788r = \text{Radius of fictitious conductor}$ 

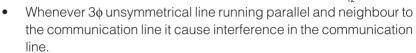
 $\rightarrow$  0.7788 times the radius of conductor

 $L_a \rightarrow L_b = L_c$  (Because of symmetry)

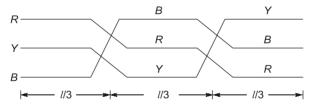
# Inductance of 3-\$\phi\$ line with unsymmetrical spacing

In this case the lines are transposed.





- In order to eliminate the communication interference transposition of line is recommended.
- Change the position of power conductor at regular interval with equidistance for a given line length, so that the position of power conductor is replaced by its successive phase conductor.



# **Advantages of Transposition**

- Net resultant flux φ, which link with communication line become zero.
- GMD/phase equal.
- L/phase equal.
- I/phase equal.
- Flux per phase equal.

Note: .....

☐ Transposition of transmission line is an old technique. The radio interference is eliminated by completely insulating any one of the phases.

......

#### Inductance of Phase-1

$$L_1 = 2 \times 10^{-7} \ln \left( \frac{D_{eq}}{r'} \right) \text{ H/m}$$

where,  $L_1 \rightarrow \text{inductance of phase 1}$ 

$$D_{\text{eq}} \rightarrow \sqrt[3]{D_{12}D_{23}D_{31}}$$
 = Equivalent spacing  
= Geometric mean of the distance of the line.

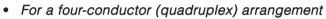
#### **Inductance of Bundled Conductor Lines**

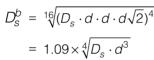
• For a two conductor (duplex) arrangement

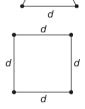
$$D_s^b = \sqrt[4]{(D_s.d)^2} = \sqrt{D_s \cdot d} \qquad \bullet \qquad d$$

• For a three conductor (tripex) arrangement

$$D_s^b = \sqrt[9]{(D_s \cdot d \cdot d)^3} = \sqrt[3]{D_s \cdot d^2}$$







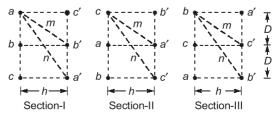
where,  $D_s^b$  = Geometric mean radius of bundled conductor

 $D_s$  = Geometric mean radius of each sub-conductor of bundle d = Spacing between the sub-conductors of a bundle

# Remember:

- ✓ Inductance of bundled conductor line is less than the inductance of the line with one conductor per phase.
- ☑ GMD depends only on the distance between the conductors and is independent of radius of conductors.

# Inductance of Double Circuit 3-0 Line



Inductance per phase per metre length

$$L = 2 \times 10^{-7} \ln \left[ 2^{1/6} \left( \frac{D}{r'} \right)^{1/6} \cdot \left( \frac{m}{n} \right)^{1/3} \right]$$
 H/phase/m

#### Mutual Inductance

Mutual inductance is defined as the flux linkages of one circuit due to the current in the second circuit per-ampere of current in the second circuit. If the current  $I_2$  produces  $\lambda_{12}$  flux linkages with circuit 1. The mutual inductance is

$$M_{12} = \frac{\lambda_{12}}{I_2}$$
 Henry

#### **Electrical Field and Potential Difference**

- The lines of electric flux originate on the positive charges on one conductor and terminate on the negative charges on the other conductor.
- If a long straight cylindrical conductor has a uniform charge throughout its length and is isolated from other charges.
- Electric field intensity E at any point,  $E = \frac{q}{2\pi c}$  V/m

 $q \rightarrow$  Charge on conductor per unit length where,

 $\in \rightarrow$  Permittivity of the medium

 $x \rightarrow$  Distance from conductor to the point under consideration.

The potential difference between two points

$$V_{xy} = \frac{q}{2\pi \in} \ln \left( \frac{D_y}{D_x} \right) \text{ Volts}$$

 $a \rightarrow \text{Charge per unit length}$ 

The potential difference between two conductor of an array of parallel conductors

$$V_{xy} = \frac{q}{2\pi \in} \ln \left( \frac{D_y}{D_x} \right) \text{ Volts } D_{am} \qquad \begin{array}{c} a \\ D_{ab} \end{array}$$
 where,  $D_x, D_y \rightarrow \text{Distance of point } x \text{ and } y \text{ from } m = 0$  charge  $q$   $q \rightarrow \text{Charge per unit length}$   $D_{bc} \rightarrow D_{bc}$ 

$$V_{ab} = \frac{1}{2\pi \in \left[ q_a \ln \frac{D_{ab}}{r_a} + q_b \ln \frac{r_b}{D_{ba}} + q_c \ln \frac{D_{cb}}{D_{ca}} + \dots + q_m \ln \frac{D_{mb}}{D_{ma}} \right]$$

# **Capacitance**

# Capacitance of Two Wire Line

$$C_{ab} = \frac{\pi \varepsilon}{\ln \left(\frac{D}{r}\right)} F/m \xrightarrow{a \bullet} D$$

where,  $C_{ab} \rightarrow \text{Line to line capacitance}$ 

 $q \rightarrow$  Charge per unit length;  $r \rightarrow$  Radius of conductor a and b

If the conductor have different radii,  $r = \sqrt{r_a \cdot r_b}$ 

where,  $r_a, r_b \rightarrow \text{Radius}$  of conductor 'a' and conductor 'b' respectively.

#### Line to neutral capacitance

$$\boxed{C_{an} = C_{bn} = 2C_{ab}} \qquad a \bullet \qquad \boxed{\begin{pmatrix} & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ & & & \\ &$$

# **Charging Current**

• The current caused by the alternate charging and discharging of the line due to alternating voltage is called **charging current** of the line.

#### Note:

Charging current flows in a line even when the line is open circuited and affects the voltage drop, efficiency and power factor of the line.

# Charging Current for 1- $\phi$ line

$$I_C = j\omega C_{an} V_{an}$$
 A/m / Phase

where,  $V_{an} \rightarrow$  Potential difference between conductor a and neutral  $\omega \rightarrow$  Frequency of alternating voltage

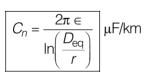
#### Capacitance of 3-\phi line with equilateral spacing

$$C_n = \frac{0.02412}{\log(\frac{D}{r})}$$
 µF/km or 
$$C_n = \frac{2\pi \in 100}{\ln(\frac{D}{r})}$$

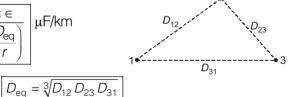
where,  $C_n \rightarrow$  Line to neutral capacitance;  $D \rightarrow$  Spacing between conductors;  $r \rightarrow$  Radius of each conductor

Charging current per phase,  $I_C = j\omega C_n V_{an}$ 

# Capacitance of 3-\$\phi\$ line with asymmetrical spacing



where,



# Capacitance of bundled conductor lines

$$C_n = \frac{2\pi \in}{\ln\left(\frac{D_{eq}}{D_{SC}^b}\right)} \text{ } \mu\text{F/km}$$

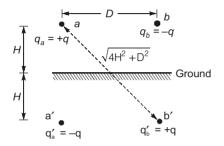
#### **Self GMD of Bundle Conductors**

- For a two conductor bundle,  $D_{\infty}^b = \sqrt{rd}$
- For a three conductor bundle,  $D_{SC}^b = \sqrt[9]{(r \times d \times d)^3} = \sqrt[3]{ra^2}$
- For a four conductor bundle,  $D_{SC}^b = \sqrt[16]{(r \times d \times d \times \sqrt{2}d)^4} = 1.09\sqrt[4]{rd^3}$

#### **Effect of Ground on Line Capacitance (Method of Images)**

The presence of ground alters the electric field of a line and hence affect the line capacitance.

#### For 1- $\phi$ line:



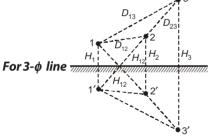
$$C_{ab} = \frac{\pi \varepsilon}{\ln \left( \frac{D}{r \left( 1 + \frac{D^2}{4H^2} \right)^{0.5}} \right)}$$
 F/m

where,

 $H \rightarrow$  Height of conductor from ground

$$C_{an} = 2C_{ab} = \frac{2\pi \varepsilon}{\ln\left(\frac{D}{r'}\right)}$$
 F/m

$$r' = r\sqrt{1 + \left(\frac{D}{2H}\right)^2}$$



$$C_n = \frac{2\pi\varepsilon}{\ln\!\left(\frac{D_{eq}}{r}\right) - \ln\!\left[\frac{\sqrt[3]{H_{12}H_{23}H_{31}}}{\sqrt[3]{H_1H_2H_3}}\right]}$$

Conductors of a 3-phase line with image charges

where,

 $H_1$ ,  $H_2$ ,  $H_3$ , and  $H_{12}$ ,  $H_{23}$ ,  $H_{31}$  are shown in figure.  $C_0$  is in  $\mu F/km$ .

#### Note:

 $\ oxdot$  Presence of ground increases the line capacitance by small amount.